

DESCRIPTION

SEALING SYSTEM FOR MEDIA-CARRYING PARTS

FIELD OF APPLICATION AND PRIOR ART

[001] The invention relates to a sealing system for media-carrying parts according to the preamble of claim 1.

[002] In order to meet the increased demands made as regards hygiene and product quality, such as e.g. the reduction in the quantity of preservatives in cosmetic products and foods, the increase in the keeping quality of dairy products and beverages, as well as in the pharmaceutical and other industries, where GMP (Good Manufacturing Practice) is a prerequisite, corresponding installations, components and parts are required, which satisfy the requirements as regards low germ content and sterility.

[003] It has been found that in particular the sealing system of the components or the like is a key aspect of such processes. As a result of ageing phenomena, external influences such as temperature, attacks by aggressive media, the seals are often damaged to such an extent that at the seal zone between the components dead volumes, clearances, etc. form, which are potential contamination sources, so that it is possible for germs, bacteria or the like to be deposited there. Thus, the nature of the seal is particularly critical. Whereas on the one hand a profile seal has been discussed, other users favour a sealing system using an O-ring.

PROBLEM AND SOLUTION

[004] The problem of the invention is to provide a detachable sealing system for media-carrying parts, which differs from conventional seals in that it has a better sealing action and consequently satisfies the constantly increasing demands made in low-germ or sterile processes.

[005] This problem is solved by the features of claim 1. Further developments of the invention form the subject matter of the subclaims.

[006] The invention proposes that the media-carrying parts have precisely complimentary sealing surfaces to one another and which are directly pressed against one another for forming a clearance-free seal. The contact surface between the sealing surfaces is limited to a narrow area directly adjacent to the media area. Unlike in the case of conventional seals, the sealing system according to the invention has no additional sealing element, such as a sealing ring or the like. Preferably it is a purely "metal on metal seal" made from the same basic material and whose sealing action is brought about

by the characteristically formed sealing surfaces on both parts, when the latter are braced against one another. A surface treatment or coating is possible, but not absolutely necessary. The complimentary sealing surfaces act in the manner of a plug and a die, which engage in one another. As opposed to conventional seals, where as a result of the material thickness of the sealing element a clearance always forms towards the media area, the seal in the present case is free from clearances. In particular the sealing clearances on conventional seals constitute potential contamination sources, because the sealing element can deform through the clearance into the media area, where a bead-like projection forms, on which residues in the form of puddles can e.g. form on emptying media-carrying pipelines and which constitute an ideal nutrient medium for bacteria or germs. This problem is obviated by the clearance-free seal of the connection according to the invention. In general, the sealing elements of conventional seals are foreign bodies, which behave quite differently to the remaining media-carrying parts. They are e.g. permanently exposed to the medium, e.g. gases or liquids and can consequently be attacked or swell, which leads to a reduction in the sealing action. They are also exposed to constant temperature changes, e.g. if the installation is steam-sterilized. For example, conventional sealing rings are only allowed up to approximately 135°C in low-germ or sterile processes. However, in the process according to the invention the seal is formed by the media-carrying parts, so that a swelling or the like is impossible.

[007] Another advantage of the sealing system requiring no elastomeric seals is that in the case of thermal sterilization the seal does not act as an insulator and the sterilization heat in the minimum time reaches all necessary areas by heat conduction.

[008] Media-carrying parts in the sense of the present application are understood to be all devices in contact with or conveying media, such as liquids or gases and which can be devices in the form of pipes, containers, fittings, valves, etc. The connections for media-carrying parts are understood to mean connections between the pipes, containers, etc. The sealing system can be a joint connection between two pipes, a pipe and a container, etc. Such connections can be screw, flange, clamp or clip connections or the like. However, it is also possible to use the sealing system for valves or the like, e.g. as a valve housing seal and/or as a spindle seal.

[009] The contact surface between the sealing surfaces of the parts is limited to an area, whose size is very small compared with the nominal width of the sealing system. The nominal width is the internal diameter of the medium area of the sealing system in millimetres and which is bounded by the medium area wall. The width of the contact surface can be a 1/5,000 to 1/50,

preferably 1/1,000 to 1/250 of the nominal width of the sealing system, e.g. 0.01 to 1 mm, preferably 0.05 to 0.2 mm. This area is directly adjacent to the media area and the sealing action of the seal consequently starts directly at the transition between the contact surface and the media area.

[010] As a result of the small dimensions of the contact surface the specific sealing pressure on pressing together the parts, is preferably in the elastic deformation range of the material of the parts. It can be close to the yield point (0.2% yield strength) of the material of the parts, e.g. 20 to 80% of the yield point value. The sealing pressure value can be approximately 30 to 140 Newton/mm². There is no cold welding of the parts, even under a high contact pressure. However, certain plastic deformations, e.g. in parts of the surfaces are possible.

[011] According to a further development of the invention the sealing surfaces can have a guide, which acts transversely to the media area, e.g. in the radial direction. As a guide, particularly in the radial direction, are preferably provided the profiled sealing surfaces of the parts. For this purpose the cross-sections of the sealing surfaces preferably have a complimentary curved profile. The profiles can e.g. be in the form of a bead and groove. However, preferably these sealing surfaces have two complimentary S-shaped profiles engaging in one another on bracing the parts. It is also possible to use interengaging trapezoidal profiles. The sealing surfaces can consequently form a type of ring spherical seal.

[012] In a further development of the invention the sealing surfaces can be designed in such a way that the specific sealing pressure decreases from the intersection line of the sealing gap with the wall of the media area. This makes it possible to prevent the sealing gap "beaking" at said intersection line leading to the formation of a clearance in which germs or bacteria could collect. As a result of the adjustable contour of the sealing surfaces it is possible to interchange parts without leaks occurring. In particular, an addition of tolerances in the dimensions of the sealing surfaces does not give rise to leaks. The sealing gap is always directly tight at its intersection line with the media area. The sealing surfaces are constructed as a type of sealing lip with a complimentary half-recess.

[013] Adjacent to the contact surface formed by the two sealing surfaces can be surface portions of both parts cut free from the contact surface, which i.e. are not in stop form on bracing the parts. However, these can serve as reserve contact surfaces, if the contact surface is enlarged away from the media area under the sealing pressure. Therefore the free-cut away from the contact surface should gradually increase. These surface portions are also preferably constructed complimentary to one another. They can pass into two plane-parallel surfaces, but preferably are also curved and preferably form

[017] The sealing system can also be a flange connection, in which the contact pressure is produced by screwing the flanges. Sealing systems constructed as joint connections are preferably welded in a pipeline or to a container, orbital welding being particularly suitable. The weld point is preferably approximately 35 to 50 mm from the sealing surfaces of the sealing

system. This is sufficient to prevent a temperature-deformation at the sealing surfaces. In addition, the relatively large diameter and the relatively high thermal capacitance inhibits heat conduction to the sealing surface. Particularly for high-grade sealing systems the heat conduction from the weld point in the direction of the sealing surfaces is low, because the high-grade steel acts as an insulator.

[018] The clearance-free seal can be used for the connection of two pipe or container parts. However, it can also be used for sealing valve components, e.g. for sealing a metal valve bellows.

[019] The parts forming the sealing system and the sealing surfaces can be made from a hard material, e.g. stainless steel. However, other materials are also suitable from which all the parts can be produced, e.g. ceramic or plastics materials.

[020] The invention also covers a process for the production of a sealing system according to one of the claims 1 to 12. The process is characterized in that the sealing surfaces can be produced by precision profile turning by means of complimentary profile cutting edges or bits. The reserve sealing surfaces can be produced at the same time using the same profile bits. The turning method can e.g. be face-turning, in which a surface located perpendicular to the workpiece rotation axis can be worked.

[021] Plastic sealing systems are preferably produced by injection moulding. The relatively small sealing surfaces can either be moulded at the same time through the use of precision injection moulding processes or can be made subsequently by precision working.

[022] These and further features can be gathered from the claims, description and drawings and the individual features, both singly and in subcombinations, can be implemented in an embodiment of the invention and in other fields and can represent advantageous, independently protectable constructions, for which protection is claimed here. The subdivision of the application into individual sections and the subheadings in no way restrict the general validity of the statements made thereunder.

BRIEF DESCRIPTION OF THE DRAWINGS

[023] An embodiment of the invention is described hereinafter relative to the attached drawings, wherein show:

Fig. 1 A part sectional view through the connection.

Fig. 2 A longitudinal section through a first part of the connection.

- Fig. 3 A larger scale representation of detail X of fig. 2.
- Fig. 4 A longitudinal section through a second part of the connection.
- Fig. 5 A larger scale representation of detail Z in fig. 4.
- Fig. 6 A part sectional representation of details X of fig. 1 and Z of fig. 3 with the connection parts joined together.

DETAILED DESCRIPTION OF THE EMBODIMENTS

[024] The sealing system according to the invention is to be illustrated in exemplified manner by means of a screw coupling 11. However other sealing system types are possible, e.g. flange, clamp or clip seals.

[025] Fig. 1 shows a screw coupling 11 such as is in particular used for the detachable connection of two pipes. The screw coupling 11 comprises three parts, namely a threaded connector 12, a collar connector 13 and a clamping device 50 in the form of a box nut 14. The threaded connector 12, collar connector 13 and box nut 14 are preferably made from stainless steel, e.g. a chrome-nickel-molybdenum steel. It is e.g. possible to use austenitic chrome-nickel-molybdenum steels of material numbers 1.4404 or 1.4435 with a 0.2% yield strength (Rp0.2) at 50°C of 182 mm². The standard nominal widths of such sealing systems are 6 to 100 mm (DN 6 to 100). The sealing systems are conventionally designed for operating pressures up to 60 bar. As a function of the diameters, they can also be designed for much higher pressures. The surfaces of the sealing systems are suitable for cleaning-in-place (CIP) cleaning and sterilization-in-place (SIP) sterilization.

[026] The threaded connector 12 comprises a pipe section 15, to which is connected a larger diameter threaded section 16. The pipe section 15 is welded to a not shown pipe. Orbital welding has proved to be a suitable welding process for sterile or low-germ processes. The transition between the threaded section 16 and pipe section 15 is conically rounded. The threaded section 16 has an external thread 17, which extends from the transition between the pipe section 15 and threaded section 16 to the end of the latter. At the threaded section-side end of the threaded connector 12 is formed a radially circumferential slit 18, which is directed towards the media area 19, i.e. towards the pipe interior. At the foot of the slit 18 are formed the sealing surfaces 20 and reserve sealing surfaces 21 of the threaded connector (fig. 6).

[027] The collar connector 13 also has a pipe section 22, as well as a flange section 23. The pipe section 23 of the collar connector is also

welded to a not shown pipe. The flange section 23 is a step-like widening on the outer surface of the pipe section 22. At the flange-side end of the collar connector, the flange section 23 has a radially circumferential, annular projection 24. At the face of the projection 24 are formed the sealing surface 25 and the reserve sealing surface 26 of the collar connector.

[028] The clamping or bracing device 50 for joining the parts is a box nut 14 in the present embodiment. It is used for bracing the threaded and collar connectors 12, 13. It has a threaded section 27 with an internal thread 28, as well as a stop collar 29 for fixing the box nut 14 to the collar connector 13. The internal thread 28 has a hard metal coating in order to prevent corrosion on screwing the box nut 14 to the threaded connector 12. In place of a threaded bracing device it is also possible to use flanges with clamping bolts, bracing clips, hydraulic clamping devices, etc.

[029] Figs. 2 and 5 show the collar connector 13 separately. The projection 24 of the collar connector 13 has a profiled face, on which are formed the sealing surface 25 and reserve sealing surface of the collar connector 13 (fig. 3).

[030] The sealing surface 25 has a curved profile in the form of a S-shape. Adjacent to the media area wall 30 is a half-recess 31, which passes into a bead-like protuberance 32. In turn, the protuberance 32 passes at its side remote from the media area 19 into a groove-like depression 33 to which is adjacent the reserve sealing surface 26. The reserve sealing surface 26 is a semicircular protuberance which, at its end remote from the media area 19, passes into a planar insertion bevel 34. The dimension of the reserve sealing surface 26 is approximately 5 to 10 times larger than the dimension of the sealing surface 25. Adjacent to the insertion bevel 34 is provided a guide section 36 of projection 24 positioned axially to the media area wall 35 and passing into a radial section 37 of the flange section 23 of the collar connector 13.

[031] Fig. 4 separately shows the threaded connector 12. At the foot of the slit 18 are formed sealing or reserve sealing surfaces 20, 21 of the threaded connector 12 complimentary to the sealing surface 25 or reserve sealing surface 26 of the collar connector 13 (fig. 5). The sealing surface 20 also has a S-shaped profile. Adjacent to the media area wall 30 is a sealing lip 37 complimentary to the half-recess 31 of the collar connector 13 and which passes into a groove-like depression 38, which is complimentary to the bead-like protuberance 32 of the collar connector. The groove-like depression 38 at its end remote from the media area 19 passes into a bead-like protuberance 39 complimentary to the groove-like depression 33 on the collar connector. The reserve sealing surface 21 is adjacent to the bead-like protuberance 39.

The reserve sealing surface 21 is a semicircular depression, which at its end remote from the media area passes into a planar insertion bevel 40. The dimension of the reserve sealing surface 21 at the threaded connector 12 is also approximately 5 to 10 times larger than the dimension of the sealing surface 20 at the threaded connector 12. Adjacent to the insertion bevel 40 is a guide section 41 of slit 18 positioned axially to the media area wall 30. At its end facing the reserve sealing surface 21, the guide section 41 passes through a further insertion bevel 42 into a radial section 43 of the threaded section 16 of the threaded connector 12.

[032] The sealing surfaces 20, 25 and the reserve sealing surfaces 21, 26 on the collar or threaded connectors 12, 13 are produced by a precision turning process, e.g. by precision face-turning. The cutting tool used can be in the form of a small flip or turnover plate, e.g. made from hard metal, which has cutting edges with the contour of the S-shaped sealing surface 20, 25 and semicircular reserve sealing surface 21, 26 and which cuts said contour into the face of the projection 24 of the collar connector 13 and to the foot of the slit 18 of the threaded connector 12. The complimentary profiled tool bits are shaped by profile grinding wheels.

[033] Fig. 6 shows the projection 24 of the collar connector 13 engaging in the slit 18 of the threaded connector 12, when the collar connector 13 and threaded connector 12 are brought together. A contact surface 44 immediately adjacent to the media area wall 30 is formed between the sealing surfaces 20, 24 of the threaded and collar connector 13. The contact surface 44 begins directly at the intersection line between the sealing gap 45 formed by the two sealing surfaces 20, 25 with the media area wall 30. The sealing lip 37 of the threaded connector 12 with the complimentary half-recess 31 of the collar connector 13 engages in stop manner. The bead-like protuberance 32 of the collar connector 13 and the complimentary groove-like depression 38 of the threaded connector 12 also engage in stop manner and consequently form the second portion of the contact surface 44. The groove-like depression 33 of the collar connector 13 and the bead-like protuberance 39 of the threaded connector 12 are not completely in stop engagement, but are instead increasingly spaced from the media area 19 on their media-side, remote flanks and consequently also form reserve sealing surfaces. For a nominal width of 50 mm, the size of the contact surface 44 is e.g. approximately 0.1 mm.

[034] The semicircular reserve sealing surfaces 21, 26 are not in stop engagement, but instead form between them an annular clearance 46. The width of the annular clearance 46 is approximately 0.05 mm in the embodiment described.

[035] To the annular clearance 46 is axially towards the media area wall 30, a separating gap 47, which is formed by the two guide sections 35, 41 of the

[0038] In the case of the screw coupling 11 shown in figs. 1 to 5, firstly the collar connector 13 is mounted on the threaded connector 12. The guide section 35 of the projection 24 is guided by the guide section 41 of the threaded connector 12 and is radially precentred. On further bringing together the collar and threaded connectors 12, 13, the complimentary constructed, profiled sealing surfaces 20, 25 engage in one another, which brings about a further radial centring, thereby preventing damage to the precision worked sealing surfaces. The collar and threaded connectors 12, 13 are brought together until the sealing surfaces 20, 25 stop-engage on the end face of the projection 24 of the collar connector 13 and on the foot of the slit 18 of the threaded connector 12. The sealing surfaces 20, 25 form a contact surface 44 bringing about a seal towards the media area 19. As a result of the separating gap 47 between the guide sections 35, 41, the two sealing surfaces 20, 25 can be mutually oriented in accurate fitting manner. In the case of damage or deformations in the front area of the sealing gap 45, the contact surface 44 can migrate radially away from the media area 19 and can consequently be subject to automatic adjustment. This is helped if the sealing surfaces are profiled in such a way that they initially contact

in the area adjacent to the media area, i.e. where the pressing action is greatest.

[039] Thus, a contact surface can form between the reserve sealing surfaces 21, 26. If the sealing surfaces 20, 25 are stop-engaged and have been oriented, the bracing of the parts can commence. For this purpose the internal thread 28 of the box nut 14 is screwed onto the external thread 17 of the threaded connector 12. The pretension is set in that the clearance 28 between the radial sections 36, 43 of the collar and threaded connectors 13, 12 is closed and the projection 24 can elastically deform. The sealing surfaces 20, 25 are so mutually oriented that the maximum contact pressure occurs at the contact area between the sealing lip 37 and the half-recess 31, i.e. directly at the transition to the media area wall 30. In the described embodiment the contact pressure is approximately 140 N/mm^2 . Due to the high contact or sealing pressure and the high precision working of the sealing surfaces with respect to the surface and radial orientation, particularly in the area of the sealing gap adjacent to the media area a clearance-free, i.e. gapless connection is formed. With respect to the roundness of the parts, a certain automatic adjustment can take place as a result of the profiling of the sealing surfaces.